

Final Focous magnet Options

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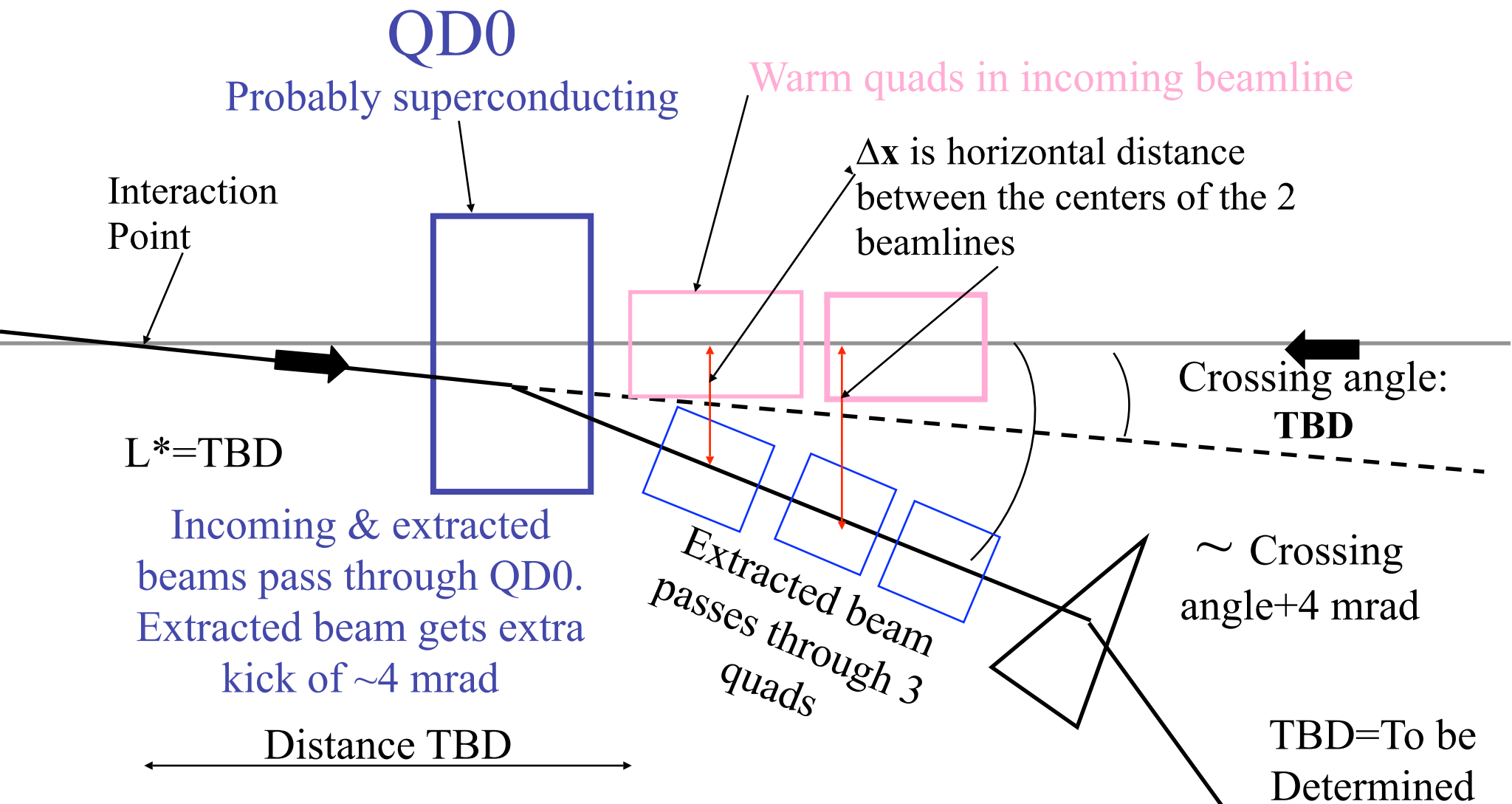
Contents

- FFQ options
 - ◆ Design choices
 - ◆ Technology choices
 - Normal magnet quadrupole
 - Superconducting magnet quadrupole
 - Permanent magnet quadrupole
 - Hybrid magnet quadrupole
 - ◆ R&D issues and Summary for FFQ
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 - ◆ Rough idea
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 - ◆ R&D issues

Design Choices

- ◆ It depends on
 - ◆ gradients for QD and QF
 - ◆ L^* and, L^{**} between QD and QF
 - ◆ crossing angle
- ◆ L^* must be determined by detector interface
- ◆ L^{**} can be very large
 - ◆ Pros : QF out of detector, shorter quads, smoother envelope, narrower SR
 - ◆ Cons : horizontal chromaticity (any other ?)
- ◆ Crossing angle?

Relative positions of the incoming & extraction magnets



Extraction quad requirements with a 20mr crossing angle.

- To minimize beam size, quad apertures and dimensions in the extraction line, the quad focusing has to start soon after the IP. Even so the beam width gets very large.
- But, the first extraction quad has to be placed at sufficient distance from IP where it can realistically fit without interference with elements of the incoming beamline.
- Two options of extraction optics are compared below - with 8 and 15 m space between IP and the first extraction quad. Lattices from Yuri Nosochkov, SLAC

Quads in 8 m option

	L (m)	GL (T)	R (mm)	Δx (mm)
Q1	5.107	254.0	20	160
Q2	7.124	-290.4	25	268
Q3	9.312	231.7	32	417
Q4	10.134	-195.0	42	609
Q5	5.765	96.8	48	818
Q6	10.102	-45.9	154	2881
Q7	9.731	41.5	164	3089

Quads in 15 m option

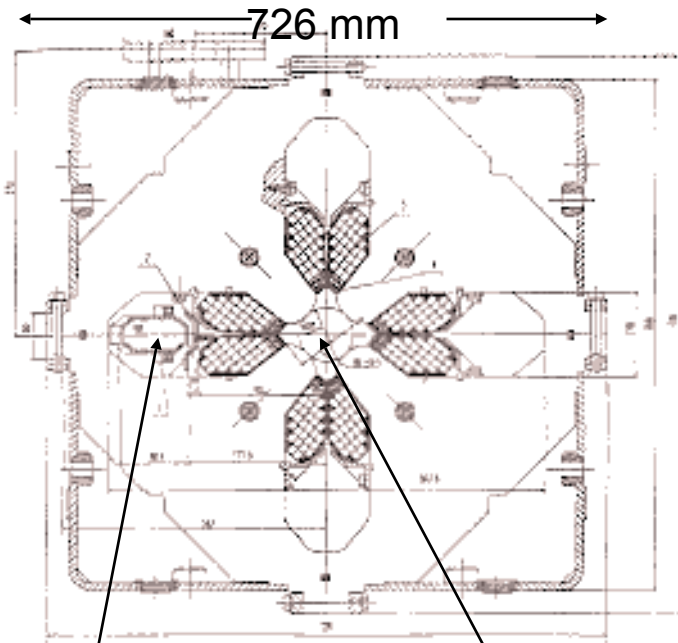
	L (m)	GL (T)	R (mm)	Δx (mm)
Q1	6.004	165.6	29	300
Q2	9.392	-216.5	35	426
Q3	9.673	185.7	42	620
Q4	11.270	-169.3	53	819
Q5	6.648	88.4	60	1051
Q6	10.717	44.8	167	3132
Q7	10.354	-40.7	178	3352

- The field in all tables is for 500 GeV/beam.
- Length L is for unsliced quad. After slicing, it is desirable to keep the same combined length of shorter quads and gaps.
- Horizontal separation Δx is between two beams at the front face of a quad, closest to IP, for 20 mrad crossing.

Unusual Quad Styles for areas with close adjacent beams

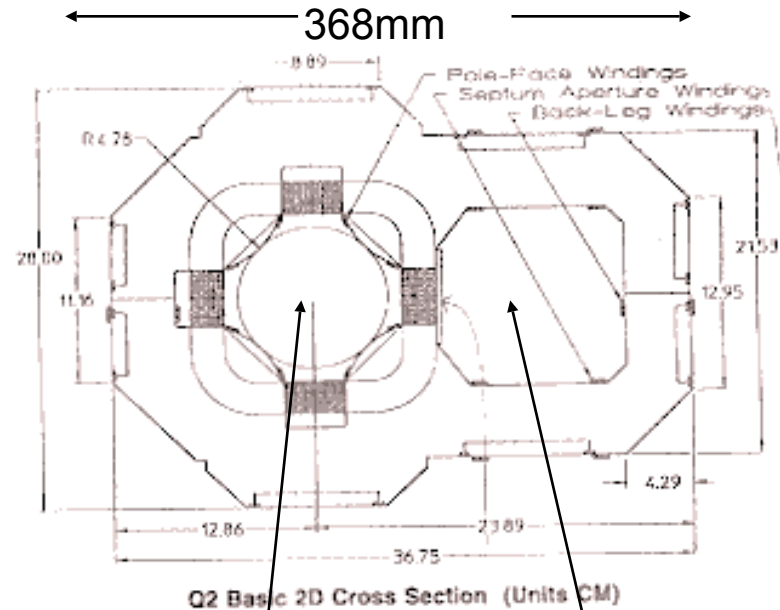
Q2 in PEP-II

Quad for HERA Luminosity Upgrade.



~221mm

Field-free region for secondary beam. Primary beam passes through center of regular quad, bore radius=35mm



~142mm

Field-free region for secondary beam. Primary beam passes through center of regular quad, bore radius=47.8mm

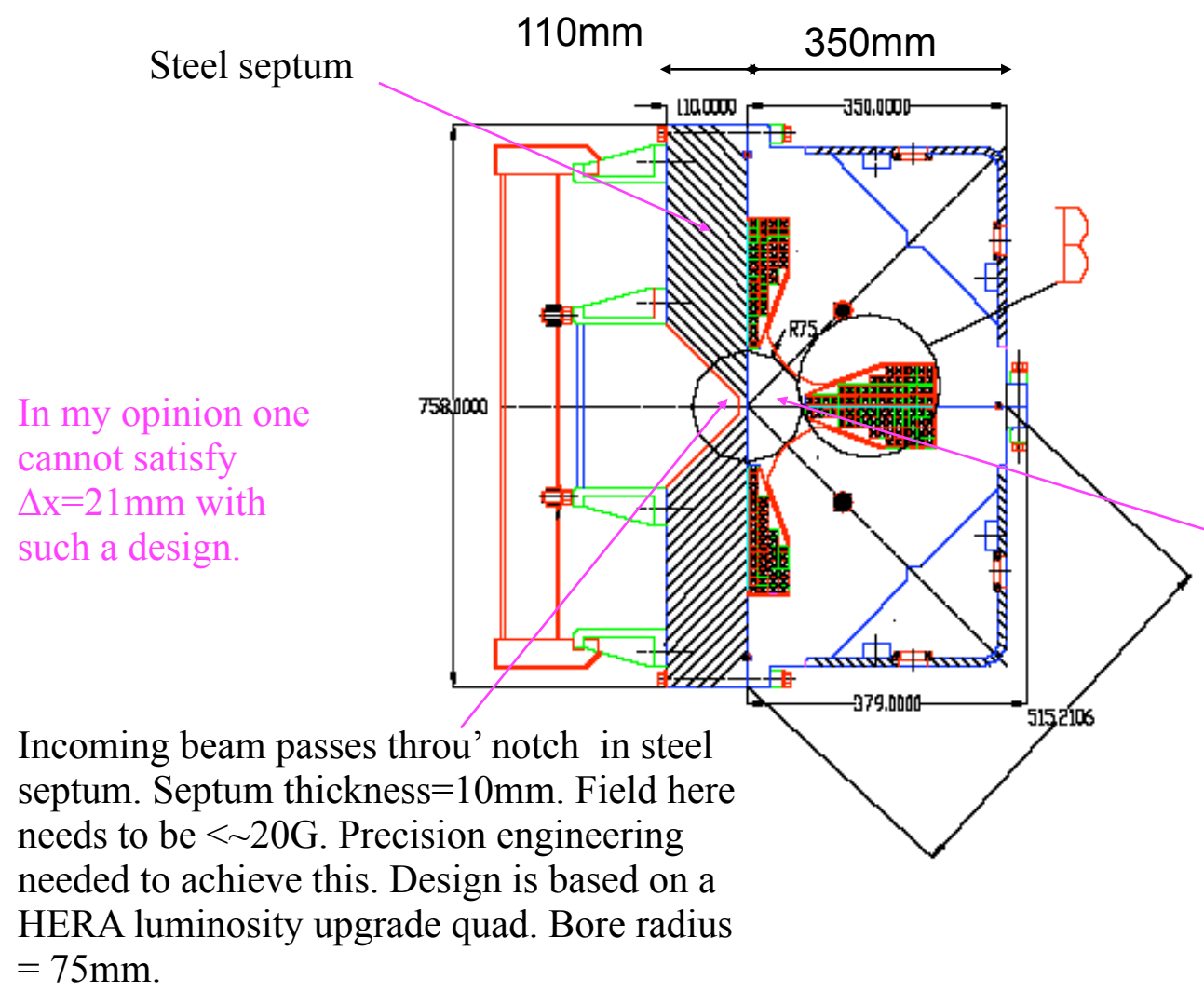
Extraction quad requirements with a 2mr crossing angle.

- If the crossing angle is only 2mr then the horizontal distance between the incoming and extracted beam, Δx , becomes even smaller, forcing even stranger quadrupole designs.
- For example, based on a **very preliminary and not fully-developed lattice** with a 2 mr crossing angle and the first extraction quad at 10m from the IP (lattice from Yuri Nosochkov) these are the requirements on the first three extraction quads, for 250Gev/beam:

Quad	L (m)	GL(T)	R mm	Δx mm
QFEX1	4.143	127.9	56	21
QDEX2	4.161	-166.4	56	52
QFEX3	2.072	82.9	63	68

This set of magnet requirements is just one of many possible sets.

Septum Half Quad from TESLA TDR for 1st extraction quad



Extracted beam passes through HALF quad to the right of its center and so beam sees a dipole field on top of the quad field. The magnet's effect on the beam shape has to be modelled using some field data from a magnet simulation program.

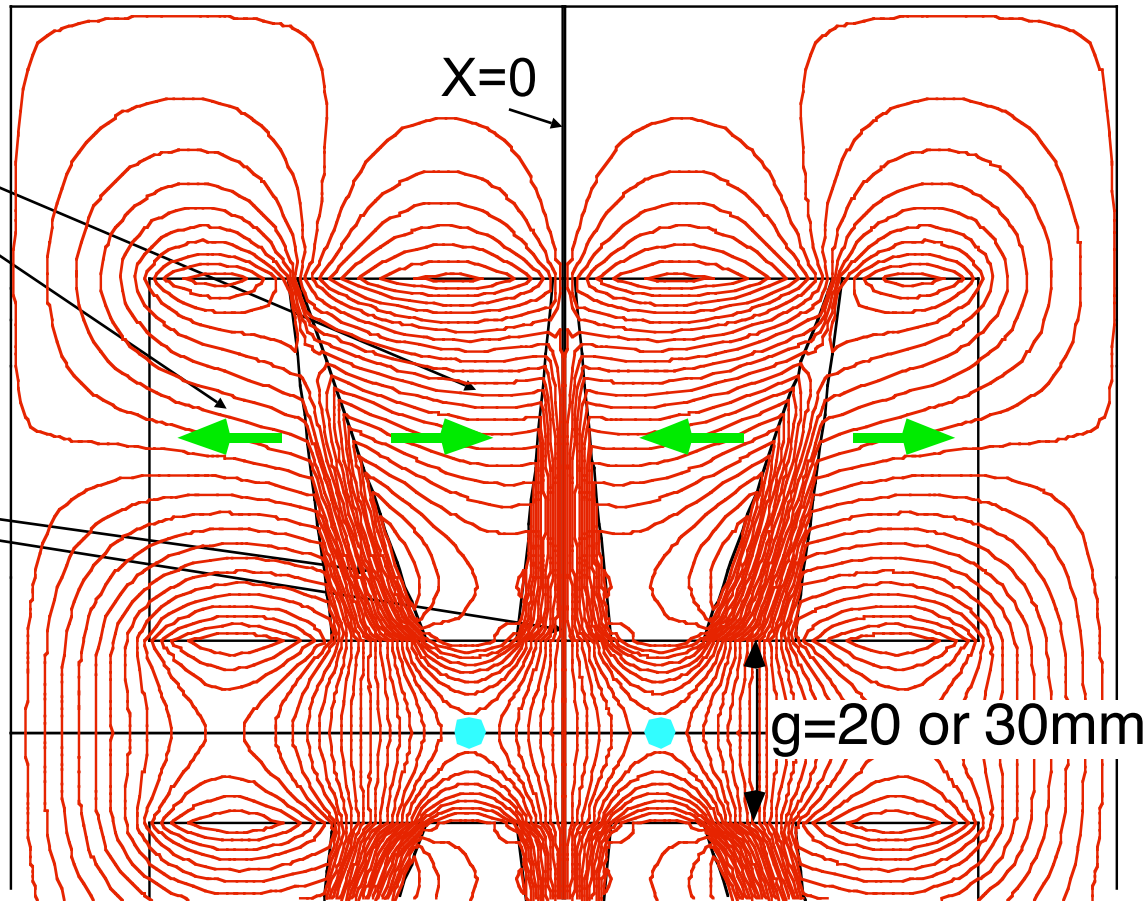
Extracted beam horizontal profile is NOT Gaussian, nevertheless outlying particles will hit face of magnet if half-aperture is too small.

Side-by-side Quads: a different approach, using permanent magnets

NEOMAX46
pm bricks

Permendur,
soft mag
material

Sides are open



Idea from
Y.Iwashita,
Kyoto
University

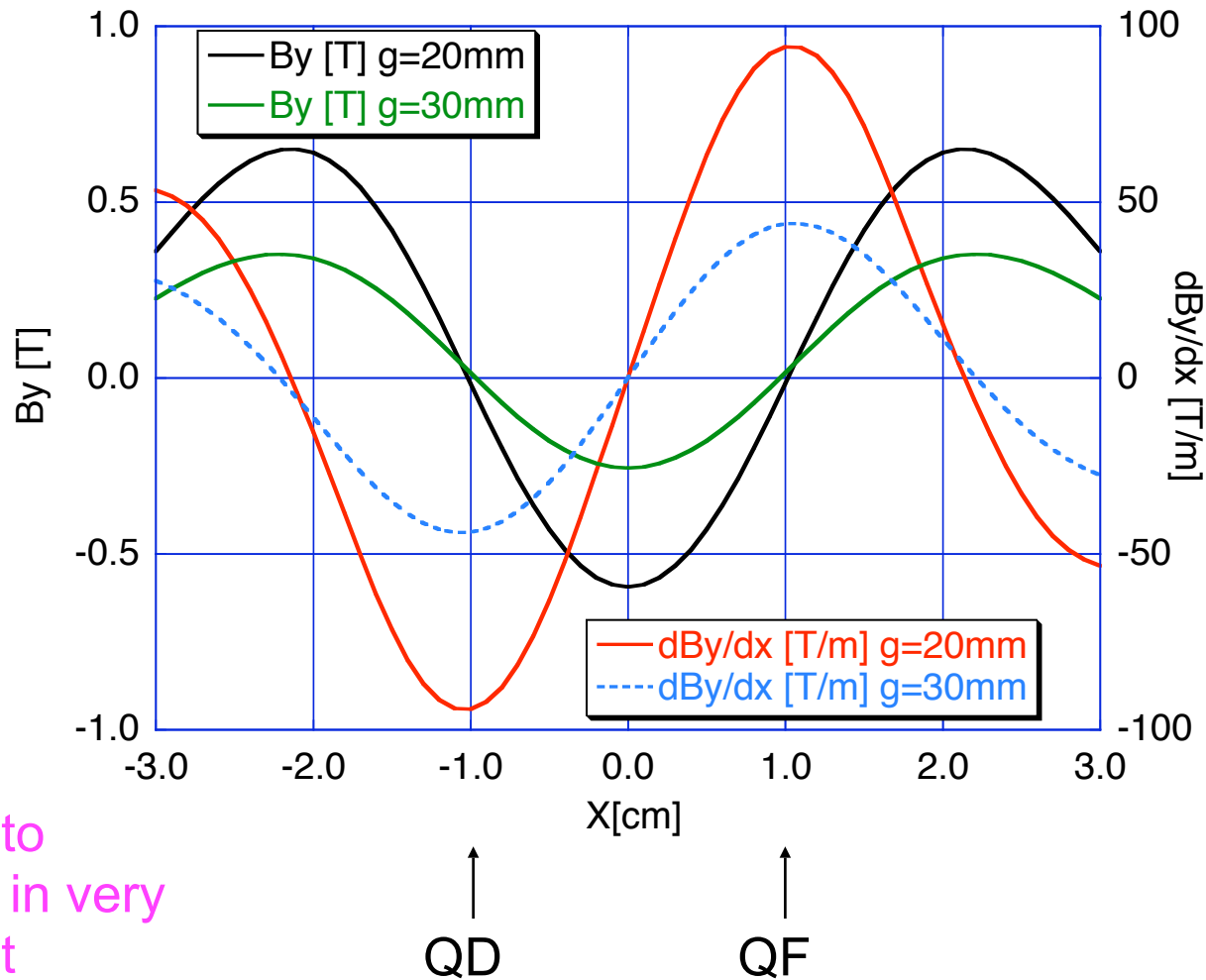
Conceptual figure.
Very preliminary.

Vary gap height to
vary gradient

Have full quad fields
in both beamlines.

20mm
Beam offset = ±10mm
QD QF

Gradient variation with x for side-by-side quads

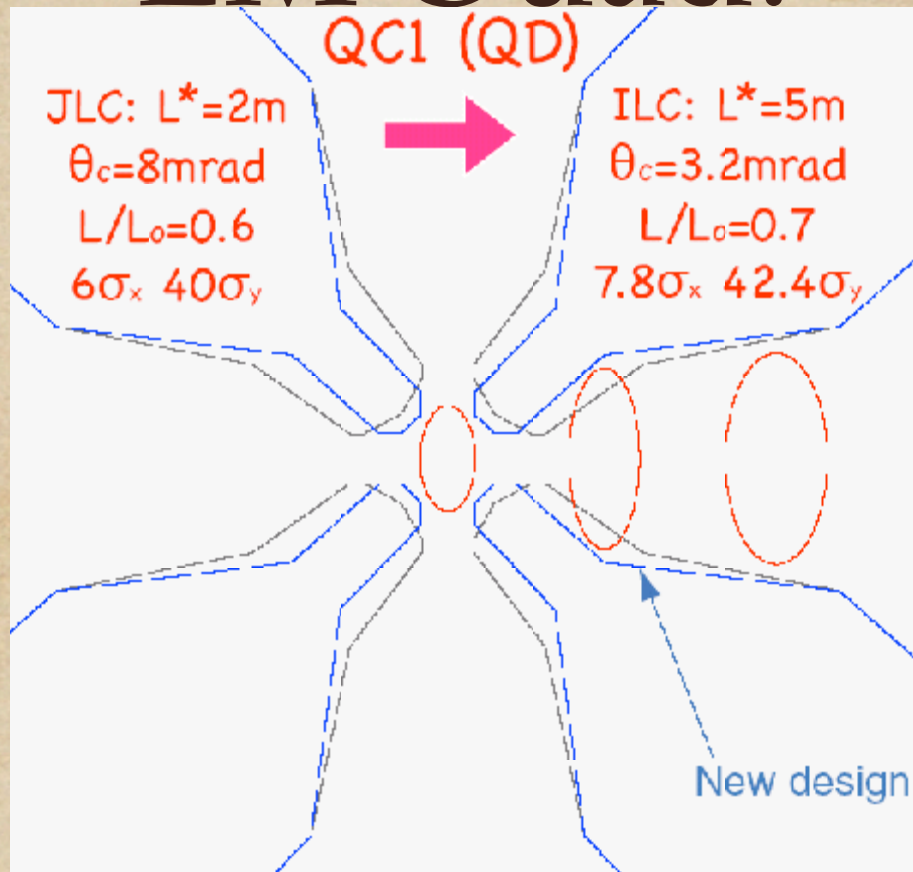


Gradient varies along x : has sextupole component.

Maximum value of $\sim 100\text{T/m}$ at $x = \pm 10\text{mm}$

Possible way to have 2 quads in very close adjacent beamlines.

EM Ouad.



Advantages

Well known technology

Disadvantages

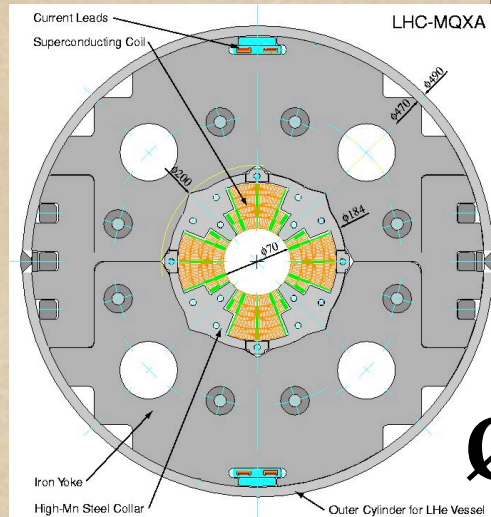
Heat Load (cooling)

	Bore radius (mm)	Effective Length(m)	Gradient (T/m)
QF1	5	3.996	44.83
QD0	1.8	3.353	-128.8

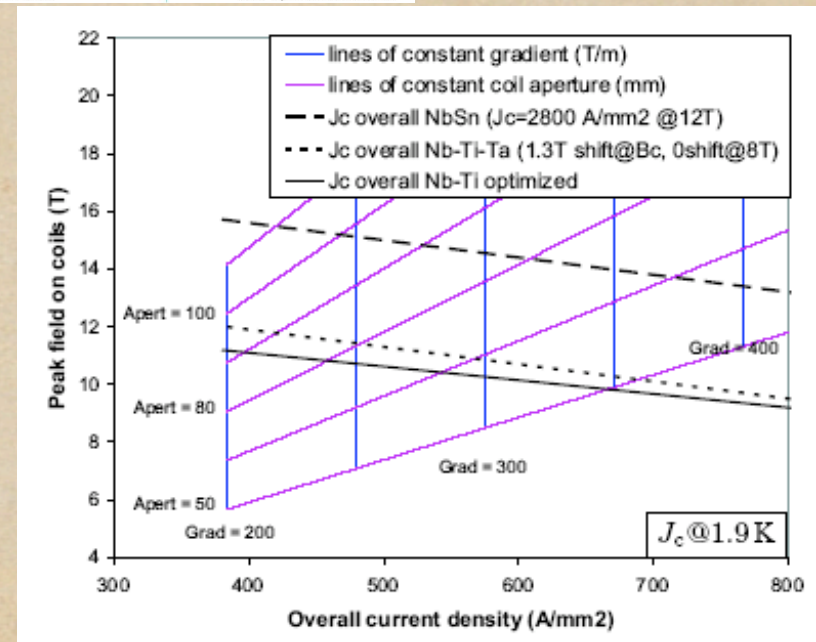
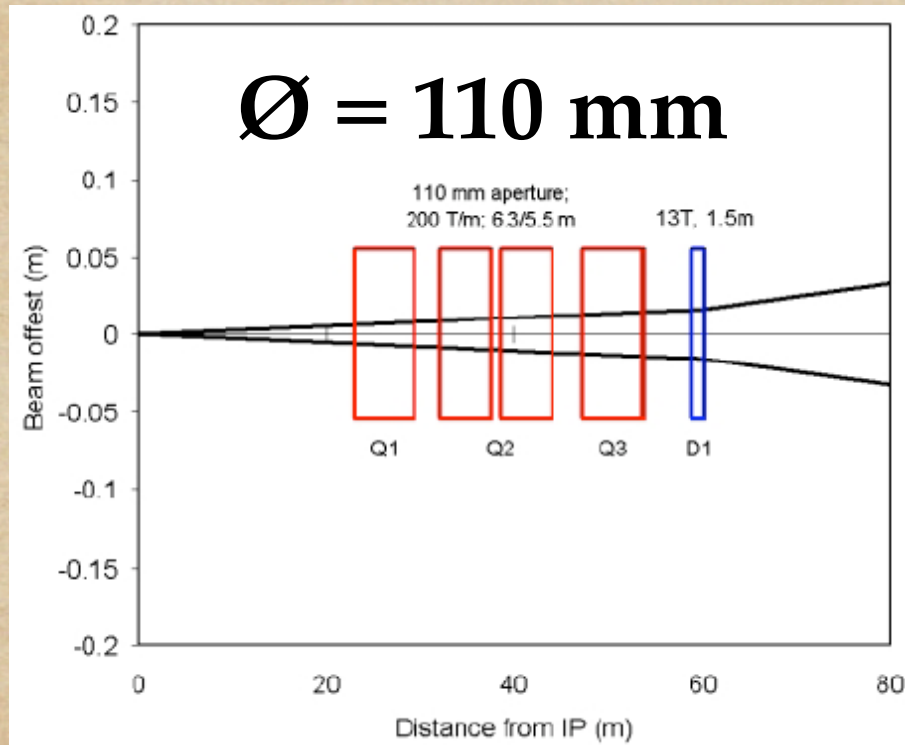
<http://acfahep.kek.jp/subg/ir/bds/jlc-bds.html#ffocus>

Larger Bores for SC quad

- ◆ LHC low beta quad
- ◆ LHC upgrades using Nb_3Sn

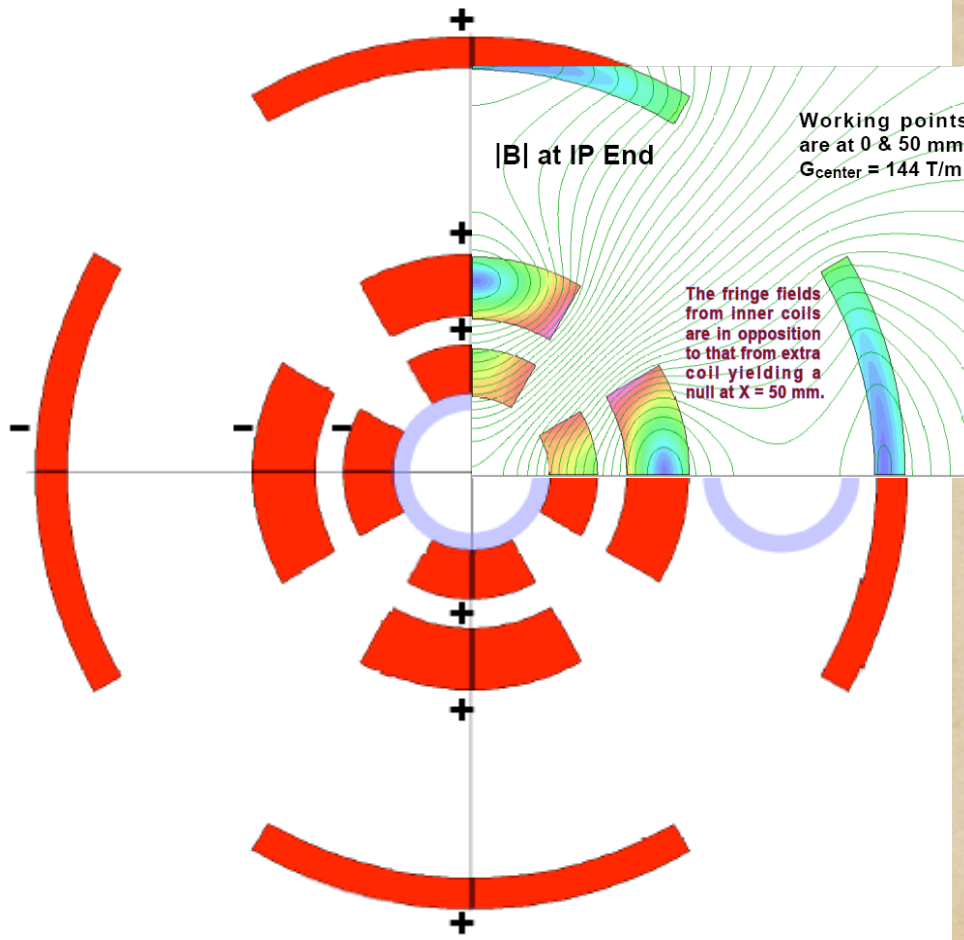


$\text{Ø} = 70 \text{ mm}$



Small bore double aperture SC quad

Cross Section at IP End with 50 mm Beam Separation



$$\text{Xing angle} = 50 \text{ mm} / L^*$$

$$G_{in} = 144 \text{ T/m}, \text{ } \varnothing_{in} = 20 \text{ mm}$$

$$G_{out} = 50 \text{ T/m}, \text{ } \varnothing_{out} = 20 \text{ mm}$$

Outer coil (single strand) is tapered to follow the exit trajectory

Outer coil can accommodate a skew quad layer

Compact SC Quad.

Inner Beam Tube 20 mm ID

Outer Cryostat Tube 114 mm OD

QDO Coil Parameters

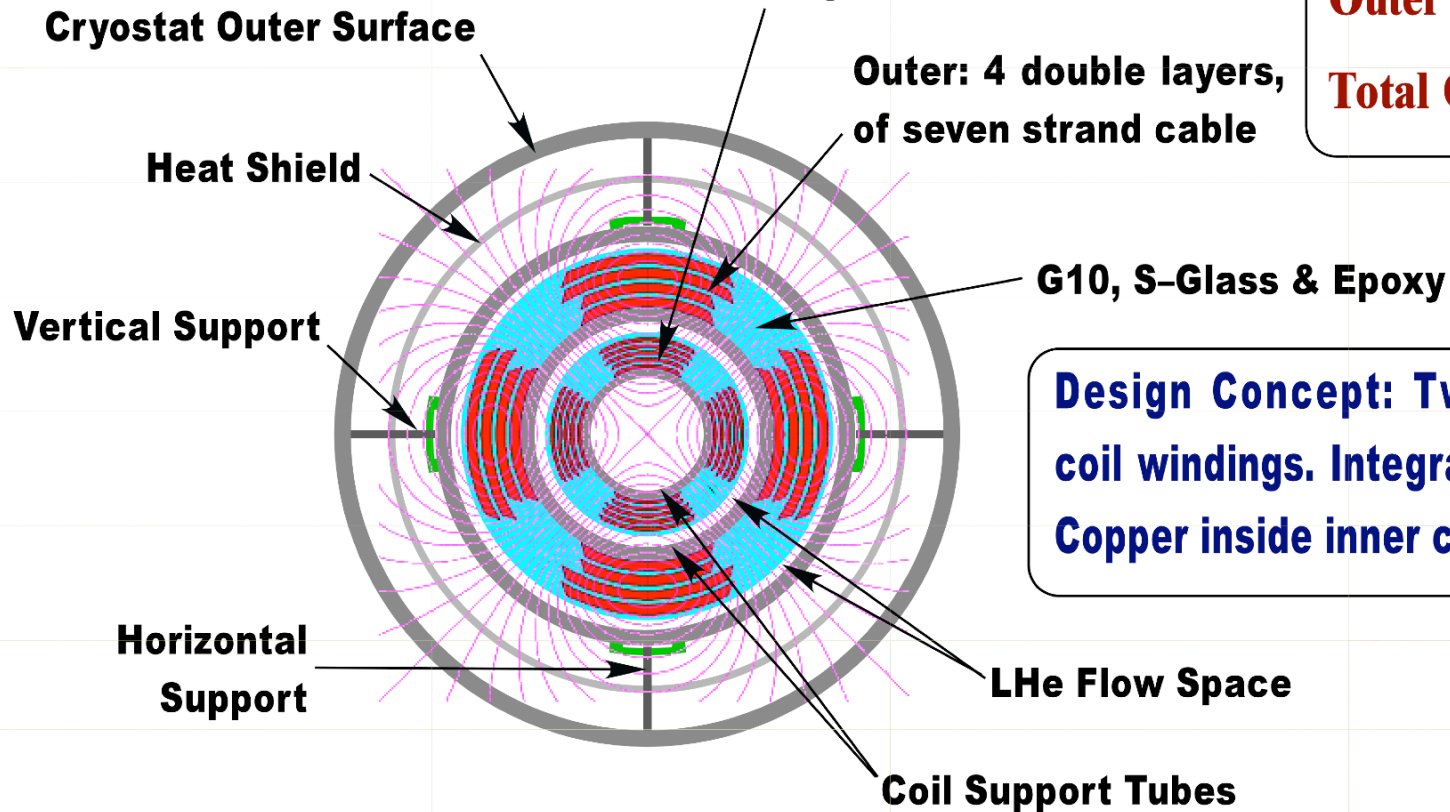
Inner Quad 63 T/m

Outer Quad 81 T/m

Total Quad 144 T/m

**Inner: 5 double layers,
single strand conductor**

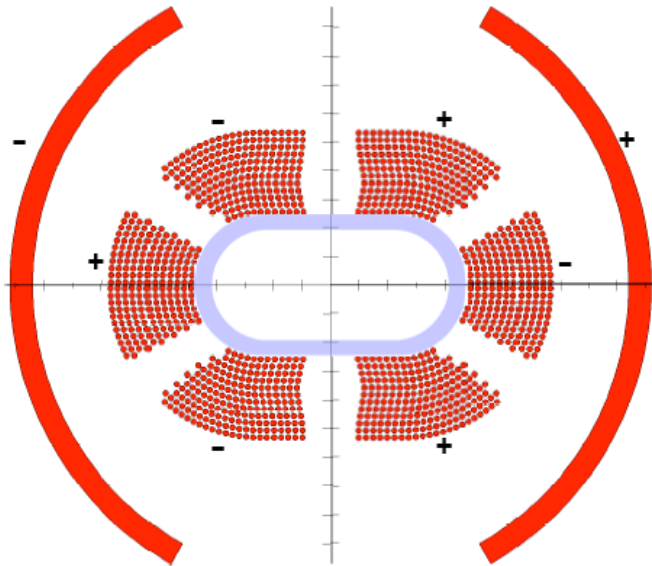
**Outer: 4 double layers,
of seven strand cable**



**Design Concept: Two independent
coil windings. Integrated helium flow.
Copper inside inner coil support tube.**

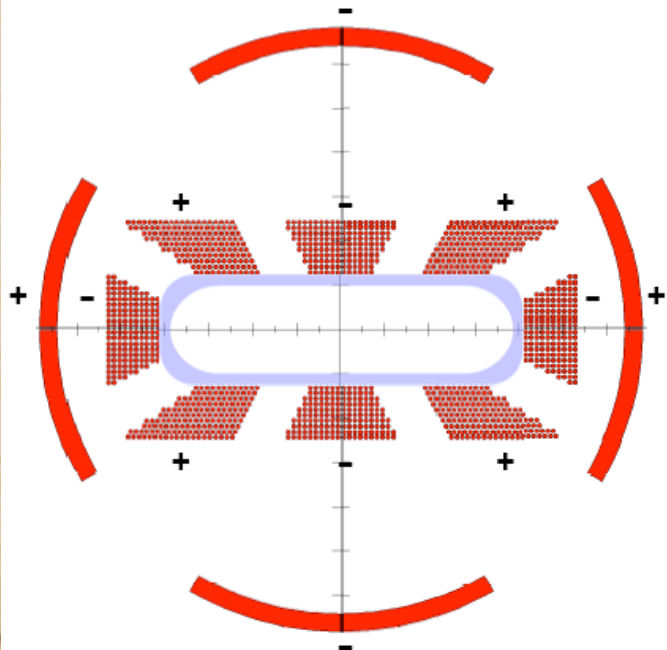
Small bore single aperture SC quad

Cross Section at IP End with Beam offsets = ± 12.25 mm



Sextupole-like : $X_{ing} = 7$ mrad
 $G = 140$ T/m

Cross Section at IP End with Beam offsets = ± 28 mm



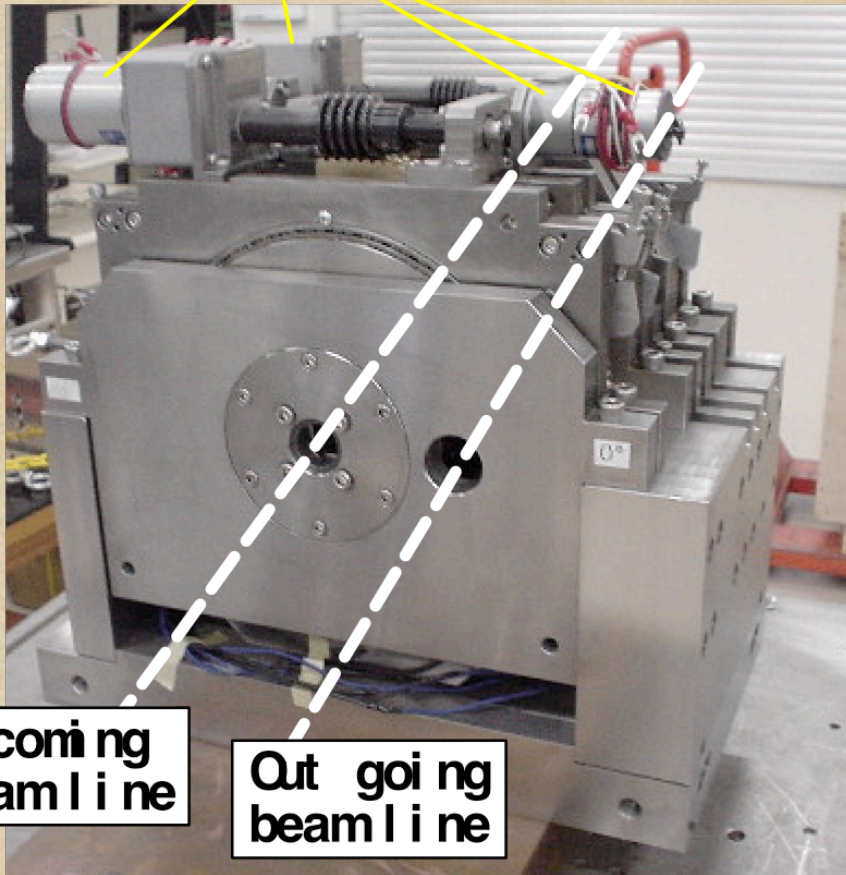
Octupole-like : $X_{ing} = 10$ mrad

Common features :

- same gradient in and out
- large non-linearities

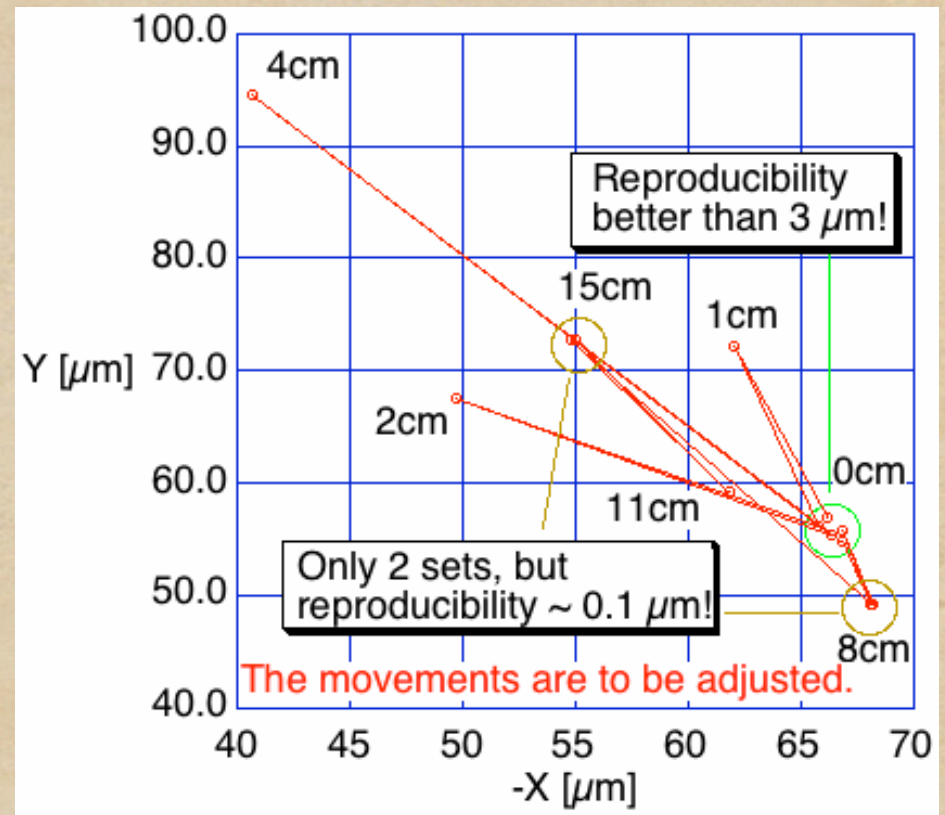
Adjustable PM Quad.

Four DC motors



Incoming beam line

Outgoing beam line



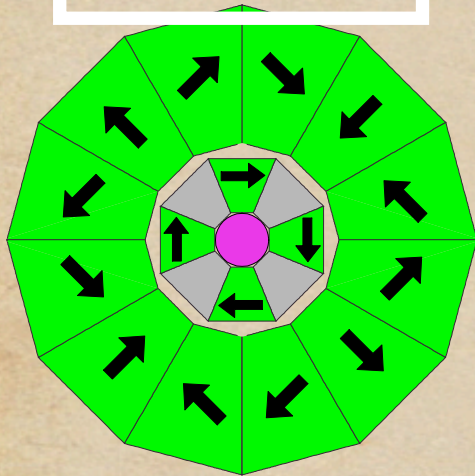
Max. Grad.	125T/m(140T/m)
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Min. Grad	23T/m(35T/m)
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PM Quad for Various L^* & X-ing Angles

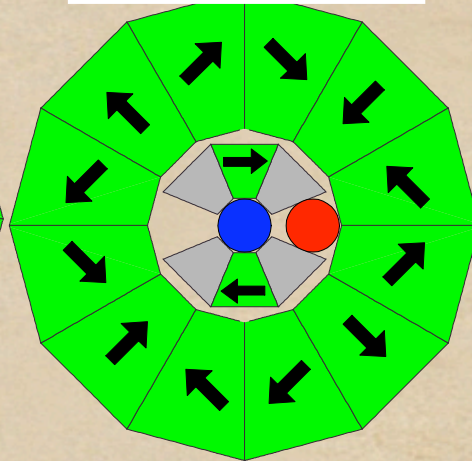
NBS

(Head on)



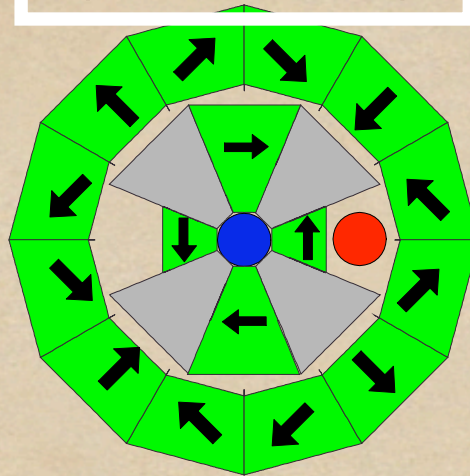
SBS

(2mrad?)



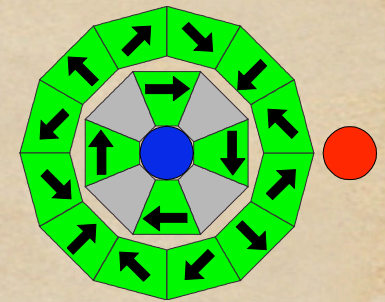
MBS

(7,13mrad?)



LBS

(20mrad?)

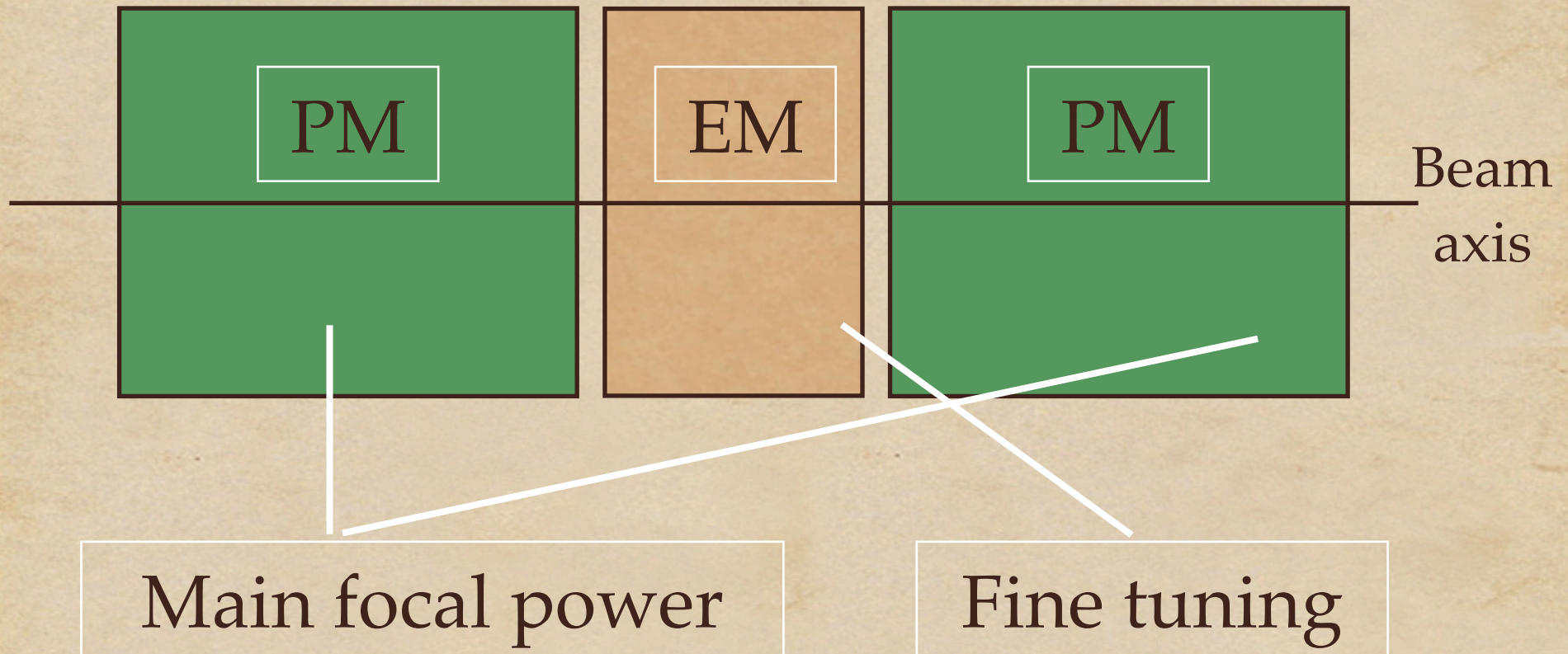


Our prototype

Q-size	$\phi 160\text{mm}$	$\phi 160\text{mm}$	$\phi 160\text{mm}$	$\phi 100\text{mm}$
$\phi 20\text{mm}$	212T/m(max) -23T/m (min)	175T/m (max) -77T/m (min)	208T/m(max) 26T/m (min)	186T/m(max) 31T/m(min)
$\phi 14\text{mm}$	296T/m	242T/m	282T/m	272T/m

NBS=No Beam Separation, SBS=Small Beam Separation
MBS=Medium Beam Separation, LBS=Large Beam Separation

Hybrid Quad. (practical option)



→ Strong tunable quadrupole!

Technology Choice

	Head on 0.3mrad	2mrad	7mrad	>13mrad
EM	<input type="radio"/>		<input type="radio"/>	
SC	<input type="radio"/>	<input type="radio"/>		<input type="radio"/>
PM	<input type="radio"/>	<input type="radio"/>	<input type="radio"/>	<input type="radio"/>

R&D

EM

- ◆ Power dissipation.
- ◆ Cooling.

SC

- ◆ Study of axis vibration
- ◆ Nb₃Sn technology
- ◆ Beam-beam losses and quad cooling

PM

- ◆ Study of radiation damage effect (PS?)
- ◆ Study of thermal effect (now preparing)
- ◆ Hybrid Q

All Qs

- ◆ Optimizing the design for each L^* , Crossing angle and bore radius.
- ◆ Optics study for optical design.
- ◆ BEAM-BEAM LOSSES
- ◆ Support and stabilisation

Summary

	EM	SC	PM
Pros.	<ul style="list-style-type: none">• Off the shelf for usual shape	<ul style="list-style-type: none">• Large Gradient• Large bore radius	<ul style="list-style-type: none">• Strong in small bore• Low power consumption
Cons.	<ul style="list-style-type: none">• Large power consumption• Lengthy	<ul style="list-style-type: none">• Axis Vibration• Beam-beam losses and quad cooling (Heat load?)	<ul style="list-style-type: none">• Stability (radiation damage, temperature coef.)

RF Kicker for Head-on-Collision

Background:

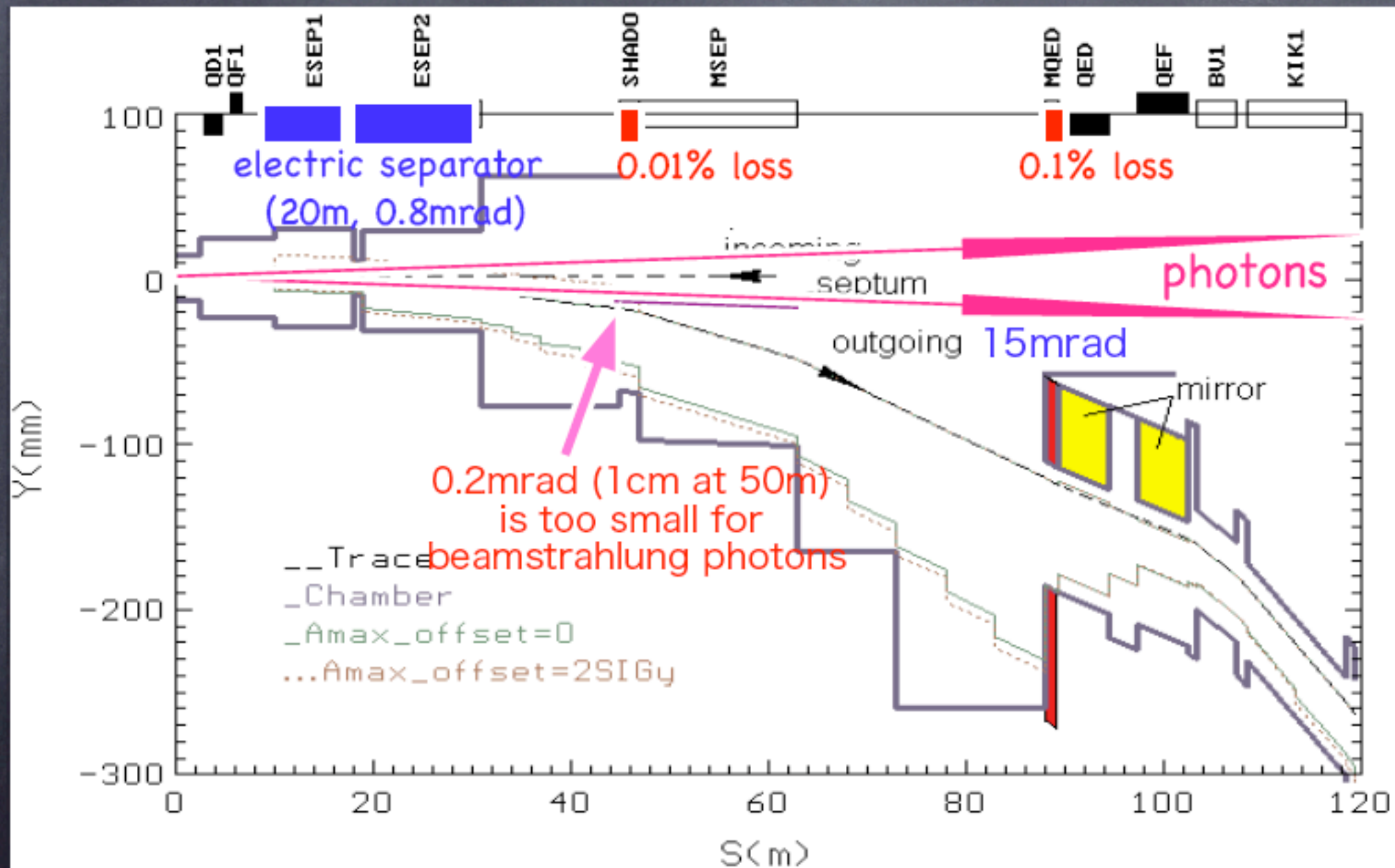
Head-on is desirable for physics,

BUT

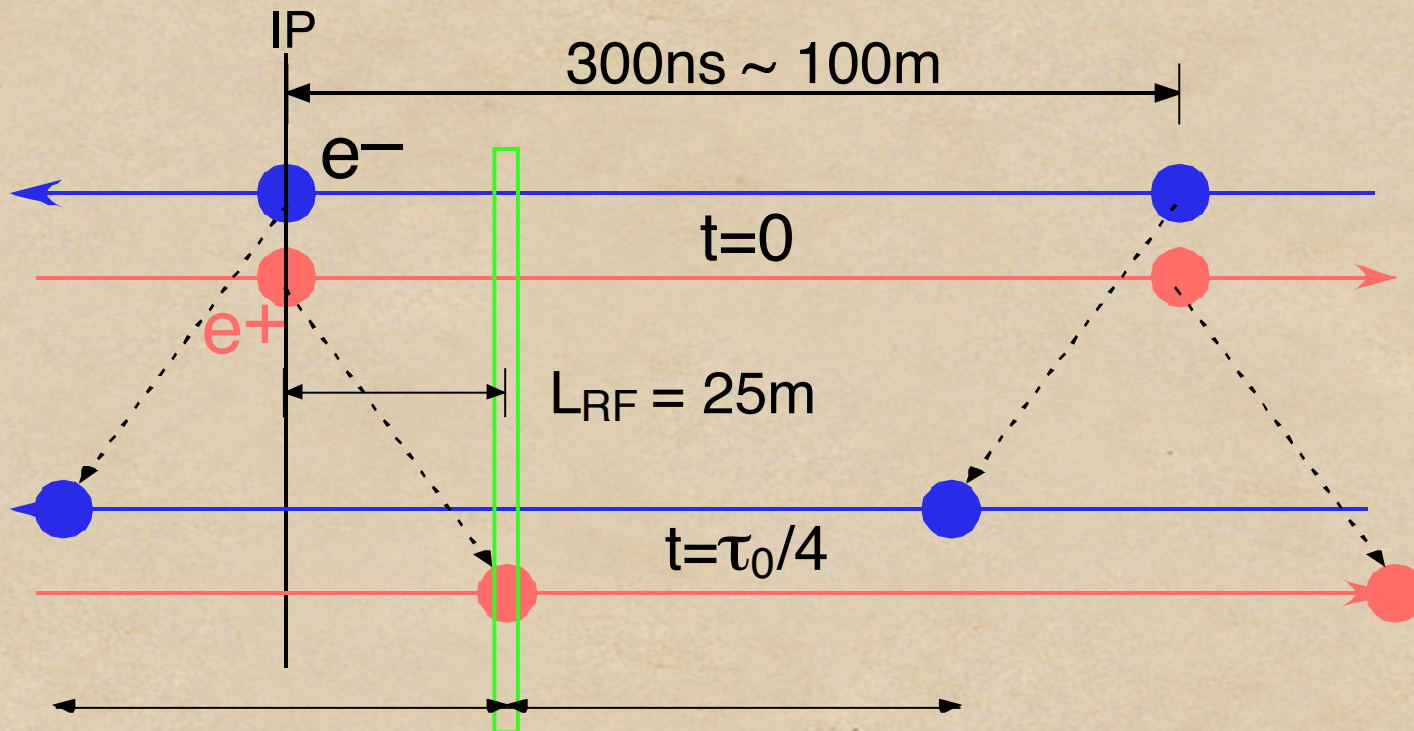
e^+ and e^- cannot be separated by

STATIC magnet

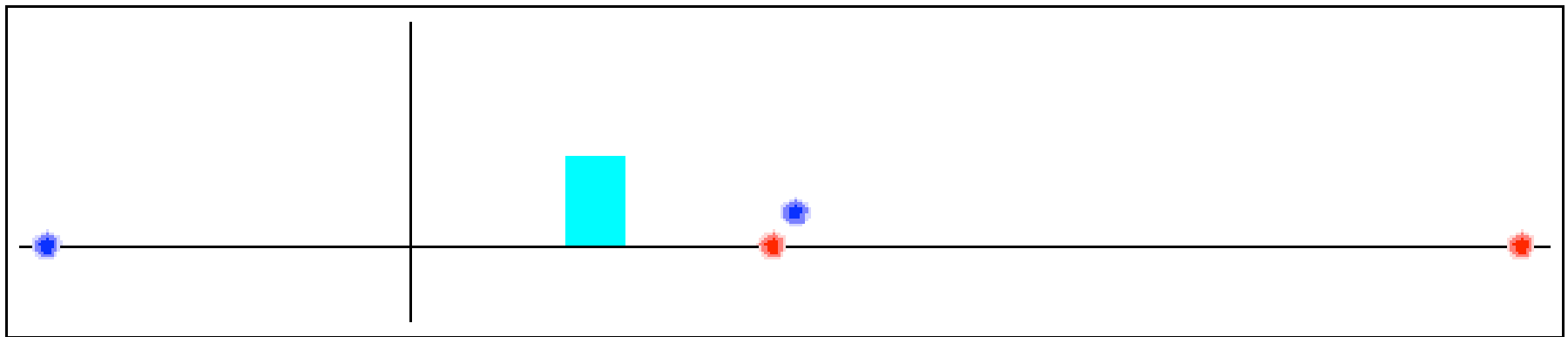
Extraction line (head-on) at TESLA-TDR



Time Structure of Beams

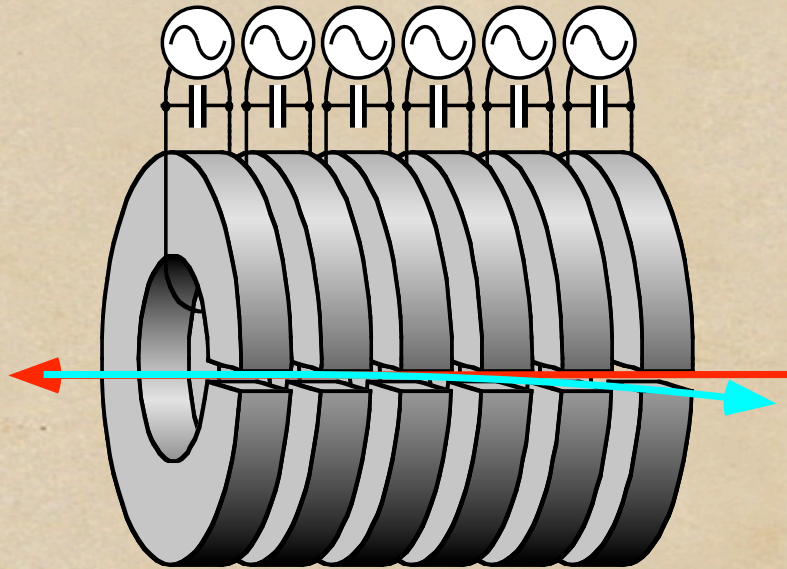


Out-bunch at the Center of In-bunch



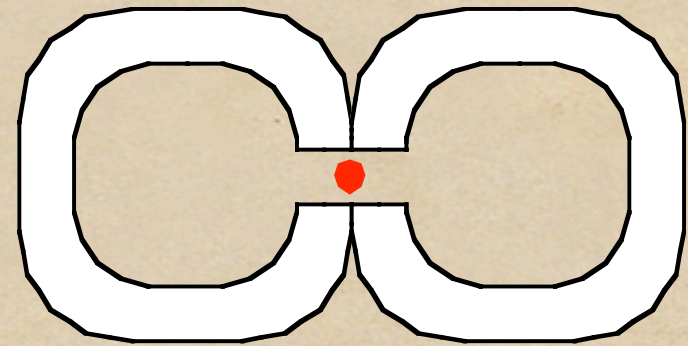
Sketch of a Kicker

DC+3MHz (+6MHz)



0.25T x L=4m
1 mrad

Variant



Double C-type

Better shielding

Step at center?

Advantage and Disadvantage

Advantage

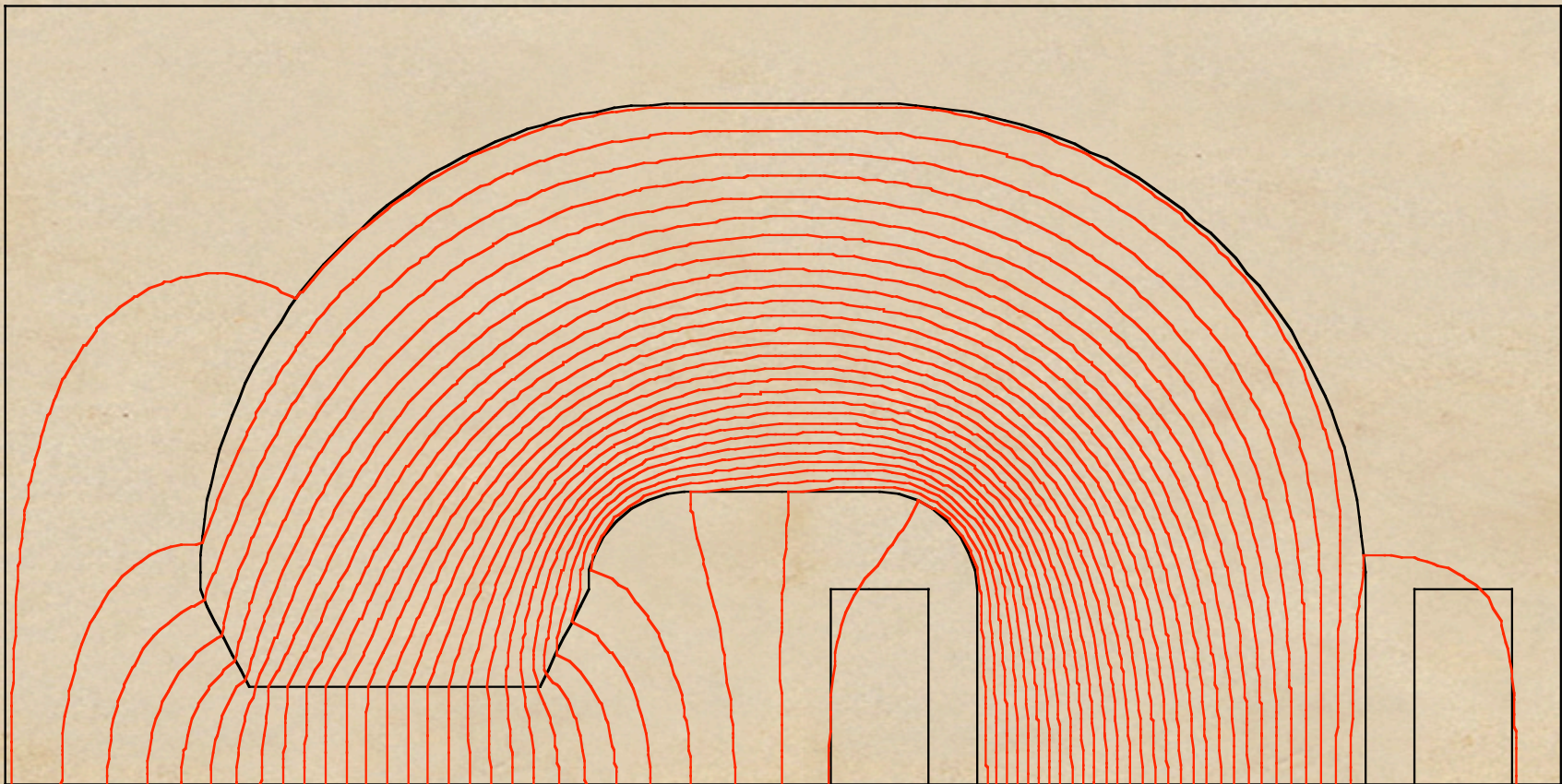
- ◆ Can attain Head-on collision.
- ◆ Easier than Crab Cavity.

Disadvantage

- ◆ If stopped, beam will hit the other side.
(Failure of all the 133 units does not likely happen.)
- ◆ It may kick the incoming beam.

RF kicker

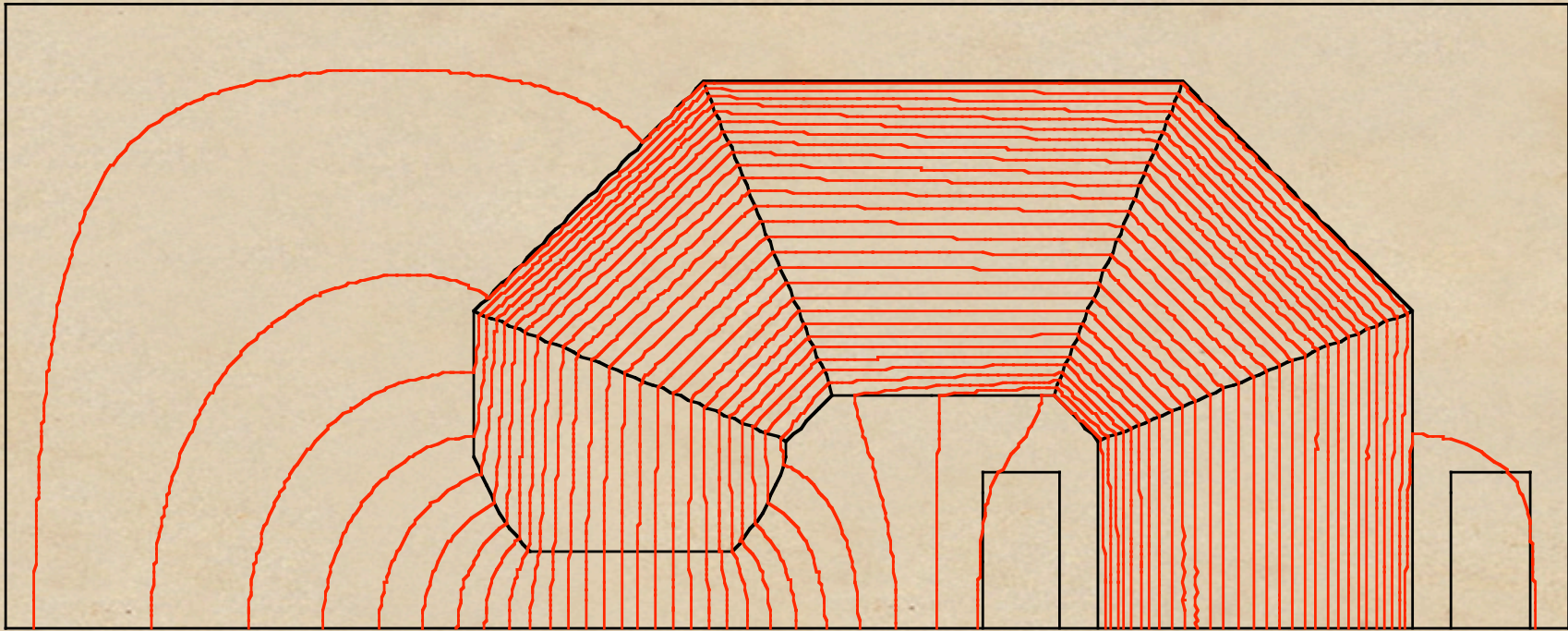
Flux plot (isotropic material)



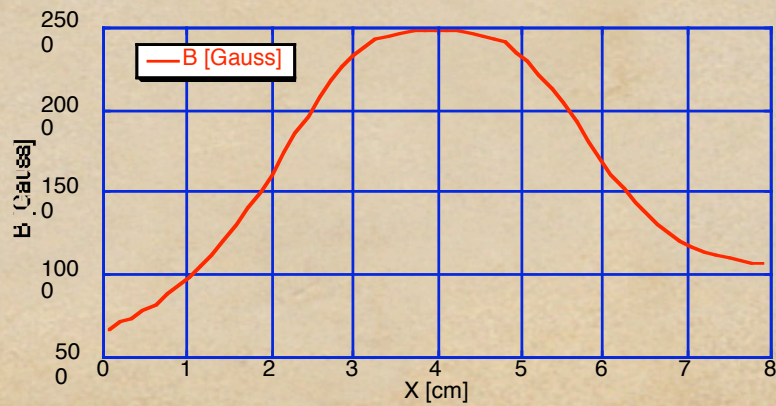
RF kicker core cut

CYCLE = 4

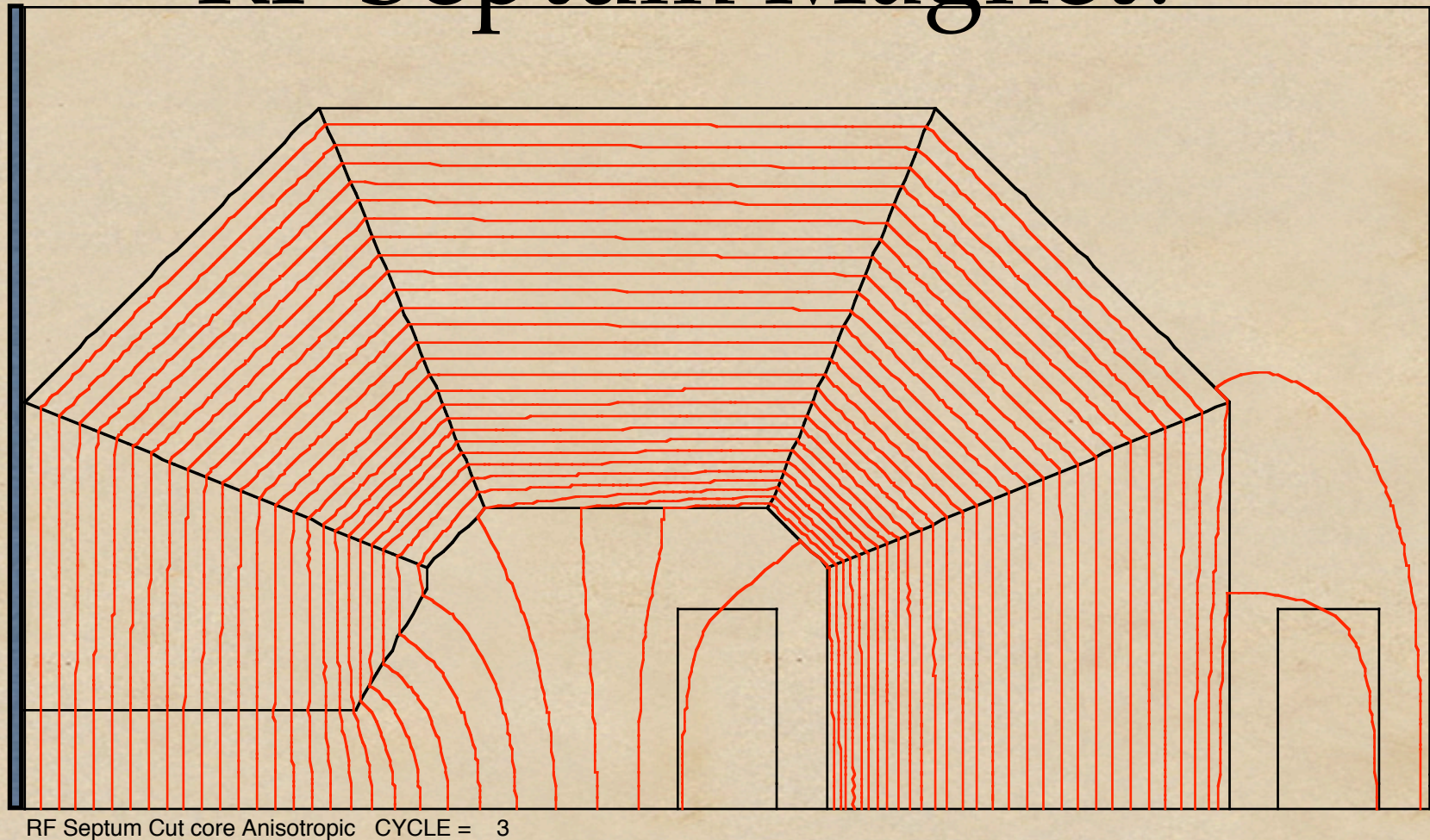
Anisotropic core (cutcore)



RF kicker Cut core Anisotropic CYCLE = 3



RF Septum Magnet?

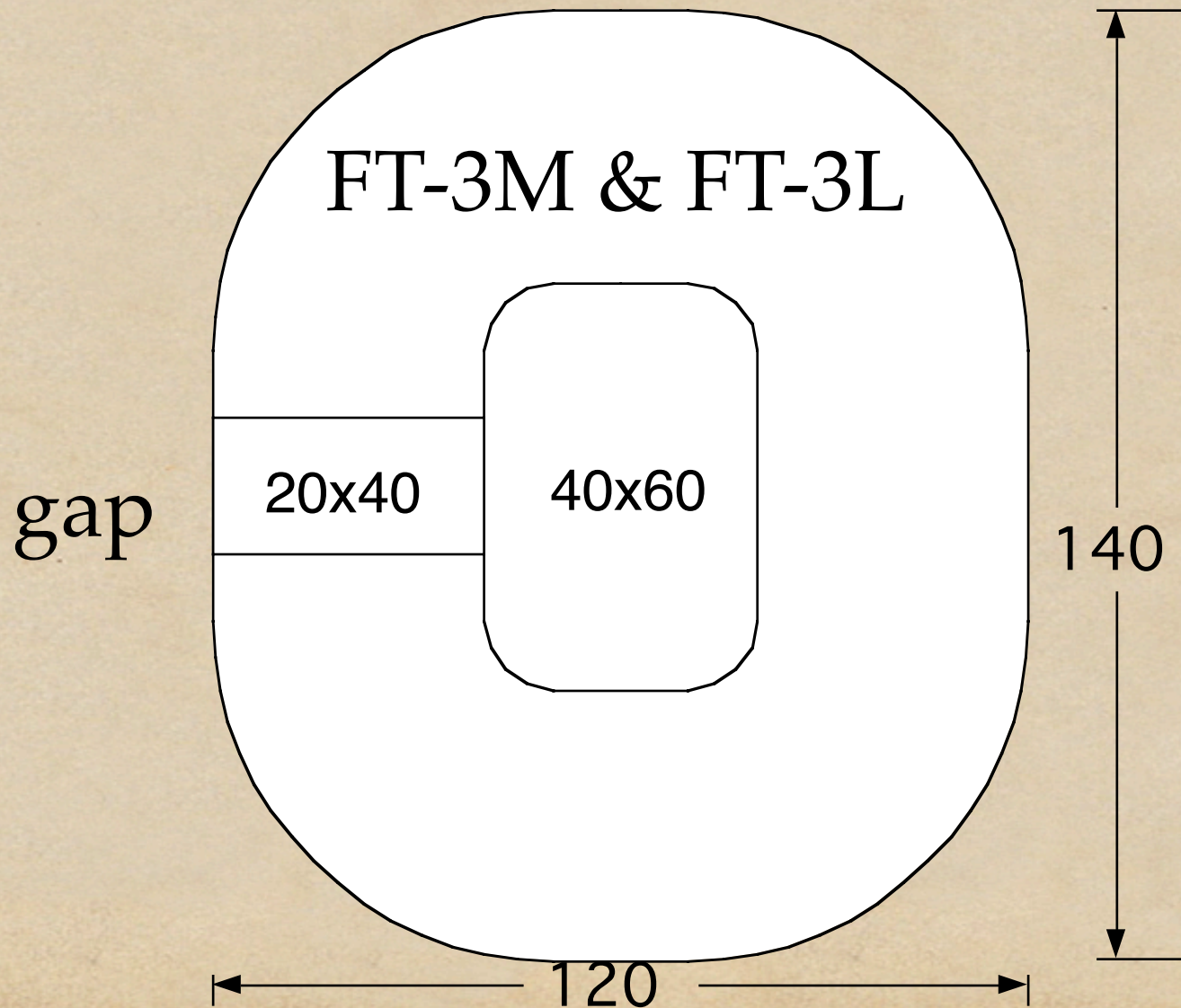


Skin depth δ : $\sim 40\mu\text{m}$ @3MHz, Cu

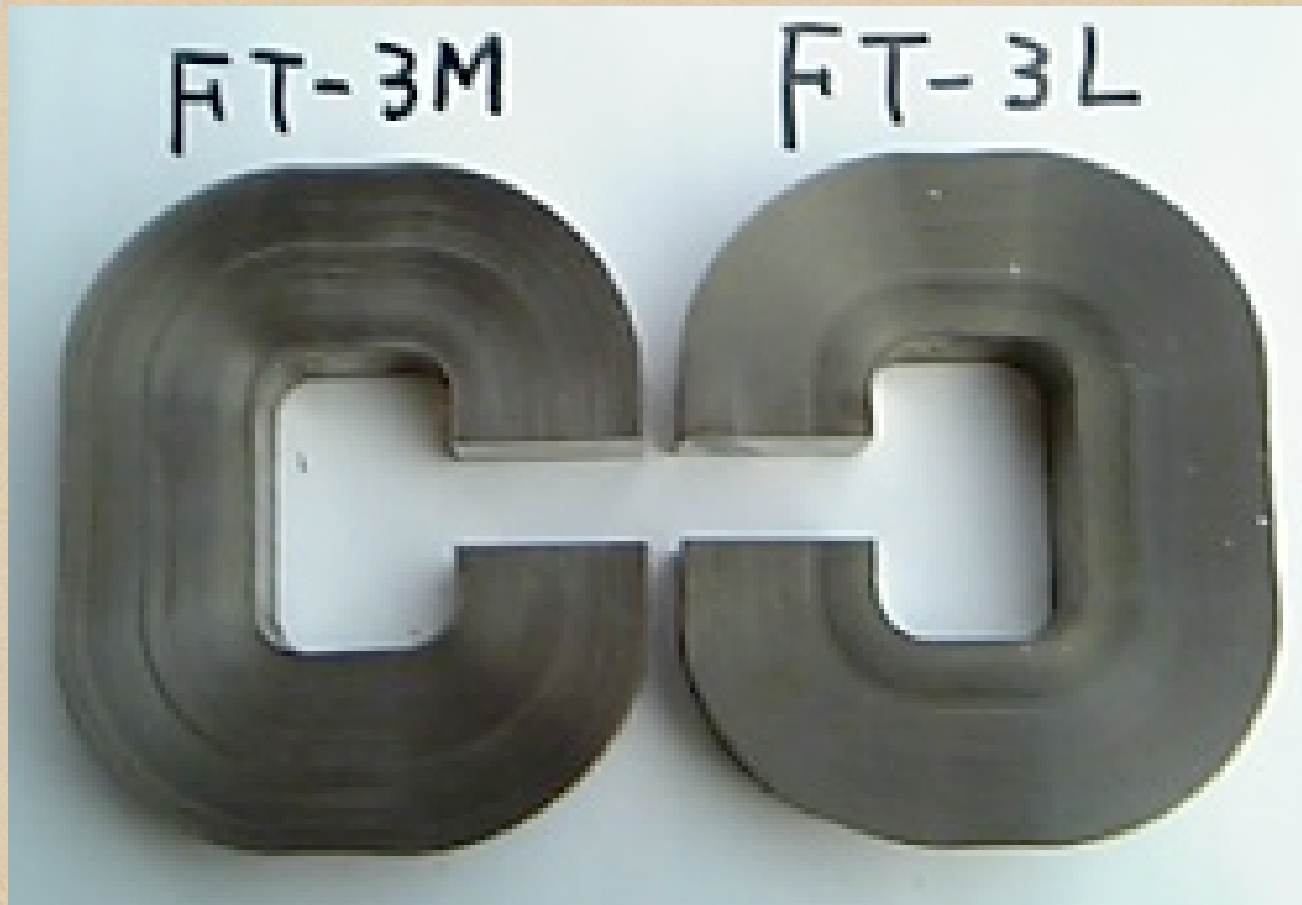
$\sigma_{\text{Cu}}=58 \text{ MS/m}$, $R\sim 2\text{m}\Omega$, $H=0.25 / \mu_0=0.2\text{MA/m}$

$P=80\text{MW/m}^2$, $4\text{m} \times 2\text{cm}=8 \times 10^{-2} \text{ m}^2 \rightarrow 6.4\text{MWpk}$

Two sample cores are ordered



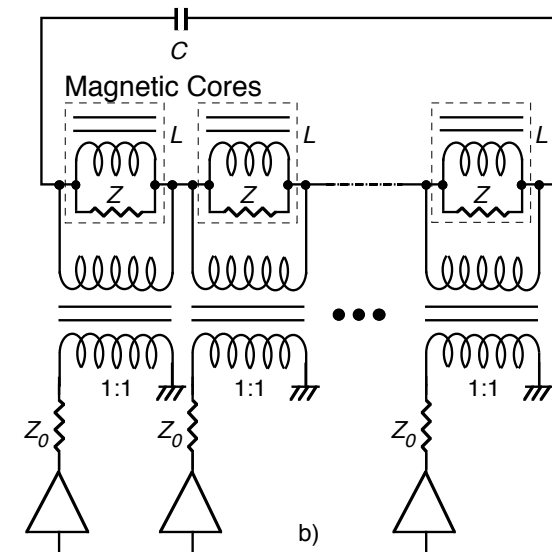
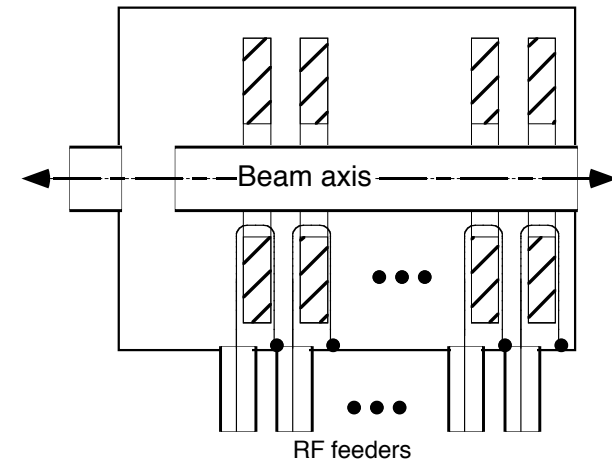
Fabricated FINEMET core
(Ready 3/1)



Untuned cavity at Kyoto U.



Led to the
excavation of
FINEMET



Multi-Feed Technique

FT-3L

【ファインメット®と従来材の磁気特性（ノーカット・トロイダルコア）】

材 料		板厚 (μm)	B_s (T)	B_r/B_s (%)	H_c (A/m)	$\mu_r(1\text{kHz})$ ($\times 10^3$)	$\mu_r(100\text{kHz})$ ($\times 10^3$)	P_{cv} (kW/m^2)	λ_s ($\times 10^{-6}$)	T_c ($^{\circ}\text{C}$)
ファインメット®	FT-1H	18	1.35	90	0.8	5.0	1.5	950	+ 2.3	~570
	FT-1M		1.35	60	1.3	70.0	15.0	350		
	FT-3H	18	1.23	89	0.6	30.0	5.0	600	≈ 0	~570
	FT-3M		1.23	50	2.5	70.0	15.0	300		
	FT-3L		1.23	5	0.6	50.0	16.0	250		
Fe基アモルファス		25	1.56	83	2.4	5.0	5.0	2200	+ 27	415
Co基アモルファス高透磁率材		18	0.55	5	0.3	115.0	18.0	280	≈ 0	180
Co基アモルファス高角形比材		18	0.60	85	0.3	30.0	10.0	460	≈ 0	210
3%Siケイ素鋼		50	1.90	85	6.0	2.7	0.8	8400	- 0.8	750
6.5%Siケイ素鋼		50	1.30	63	45.0	1.2	0.8	5800	- 0.1	700
50%Niパーマロイ		25	1.50	95	12.0	—	—	3400	+ 25	500
80%Niパーマロイ高透磁率材		25	0.74	55	0.5	50.0	5.0	1000	≈ 0	460
80%Niパーマロイ高角形比材		25	0.74	80	2.4	—	—	1200	≈ 0	460
Mn-Znフェライト高透磁率材		—	0.44	23	8.0	5.3	5.3	1200	- 0.6	>150
Mn-Znフェライト低損失材		—	0.49	29	12.0	2.4	2.4	680	- 0.6	>200

注1) B_s 、 B_r/B_s 、 H_c ：直流磁気特性 ($H_m=800\text{A}/\text{m}$, 25°C)、 $\mu_r(1\text{kHz})$ ：比透磁率 (1kHz, $H_m=0.05\text{A}/\text{m}$, 25°C)、

$\mu_r(100\text{kHz})$ ：比透磁率 (100kHz, $H_m=0.05\text{A}/\text{m}$, 25°C)、 P_{cv} ：コアロス (100kHz, $B_m=0.2\text{T}$, 25°C)、 λ_s ：飽和磁歪定数、 T_c ：キュリー温度

注2) 上記特性は、当社での測定による

High B, low core loss, high Tc

Power Estimation

Stored Energy for a core : $W=0.75$ [J]

Coil current for 0.25T : $I = 4$ [kA]

Inductance ($L I^2 / 2 = W$) : $L = 94$ [nH]

Capacitance ($L C = \omega^{-2}$) : $C = 30$ [nF]

Voltage ($C V_c^2 / 2 = W$) : $V_c = 7$ [kV]

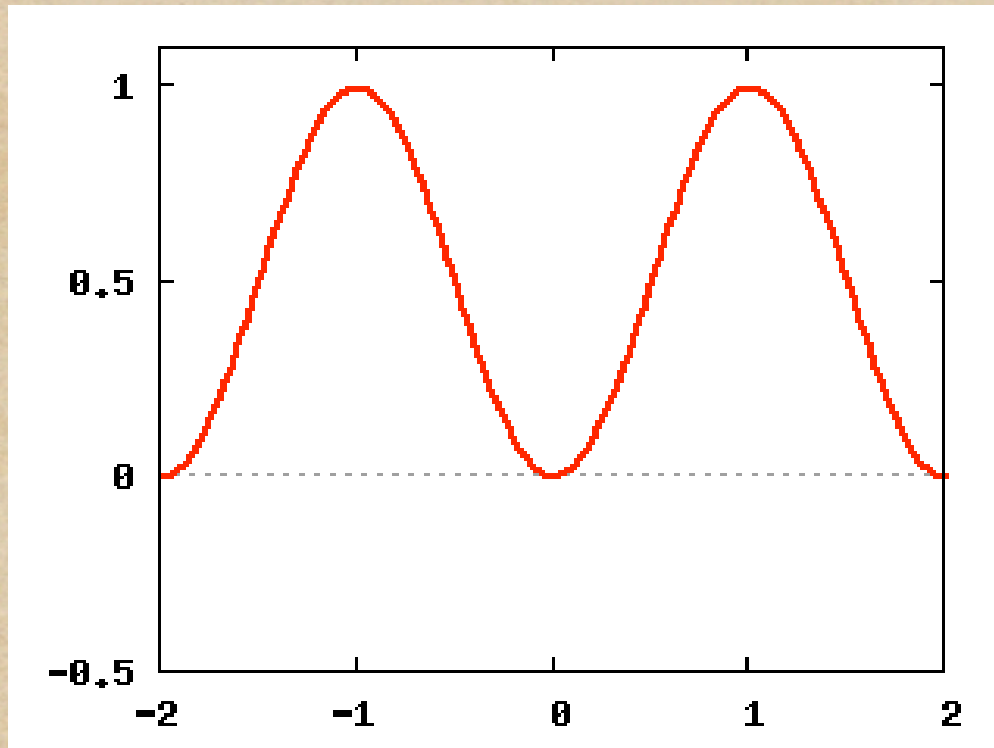
Core Volume : $C_v = 300$ [cc]

Core Loss P_{cv} (3MHz, 0.2T) : $P_{cv} = 10^8$ W / m³

Core Loss P (3MHz, 0.25T) : $P = 45$ kW / core

Waveform 1: simple cosine

$$f(t) = 1 - \cos(\omega t)$$



Phasing

division ≥ 4

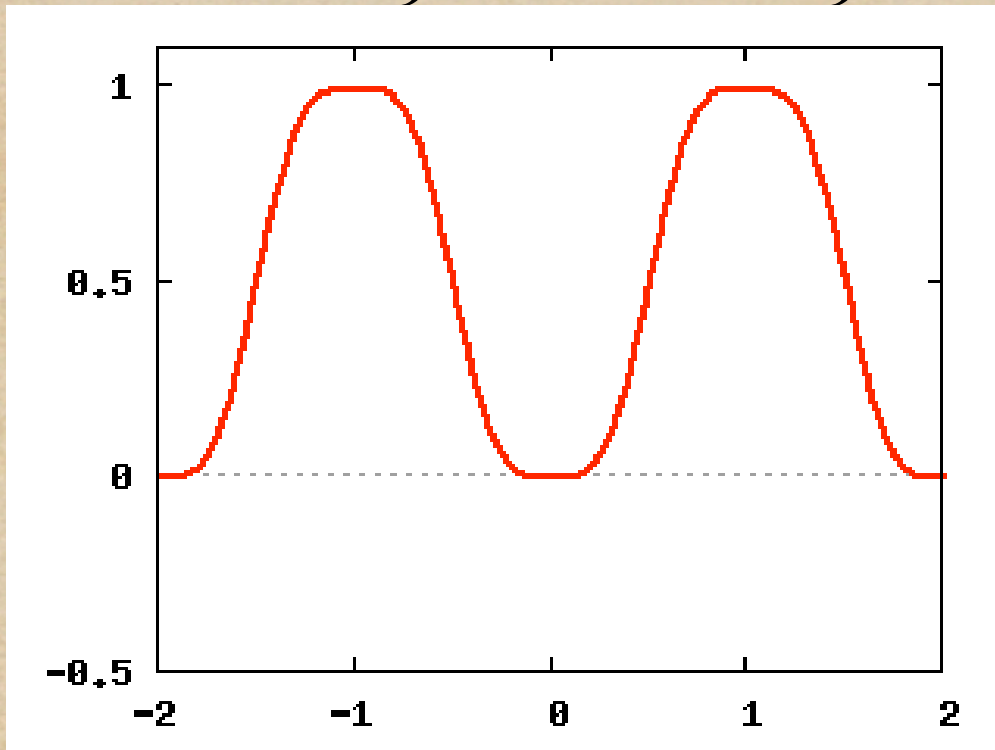
1 Section = 1.0m

Both end $x =$
0.50m

A $- 2.17 \times 10^{-7}$

Waveform 2: two cosines

$$f(t) = \frac{8}{9} - \cos(\omega t) + \frac{1}{9} \cos(3\omega t)$$



Phasing division ≥ 1

$$x = 2.0\text{m}$$

$$\theta_x = 4.65 \times 10^{-8}$$

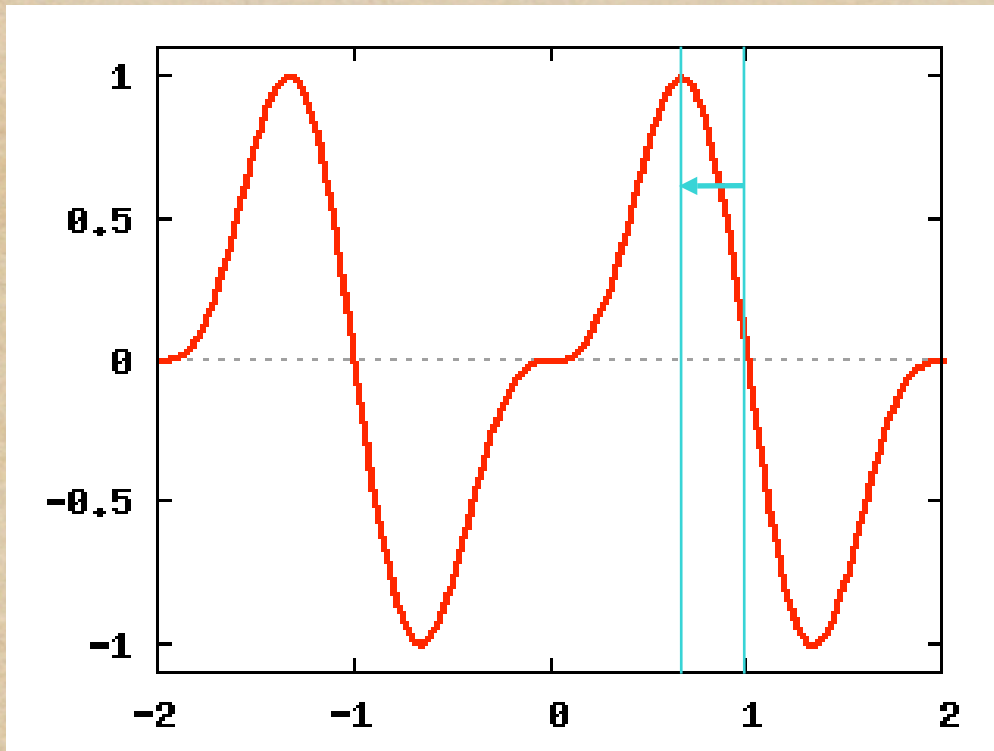
$$< 3.0 \times 10^{-7}$$

Very flat base.

But difficult?

Waveform 3: sines

$$f(t) = -\sin(\omega t) + \frac{1}{2}\sin(2\omega t)$$



Phasing division ≥ 2

$$x = 1.0\text{m}$$

$$\theta_x = 9.54 \times 10^{-8}$$

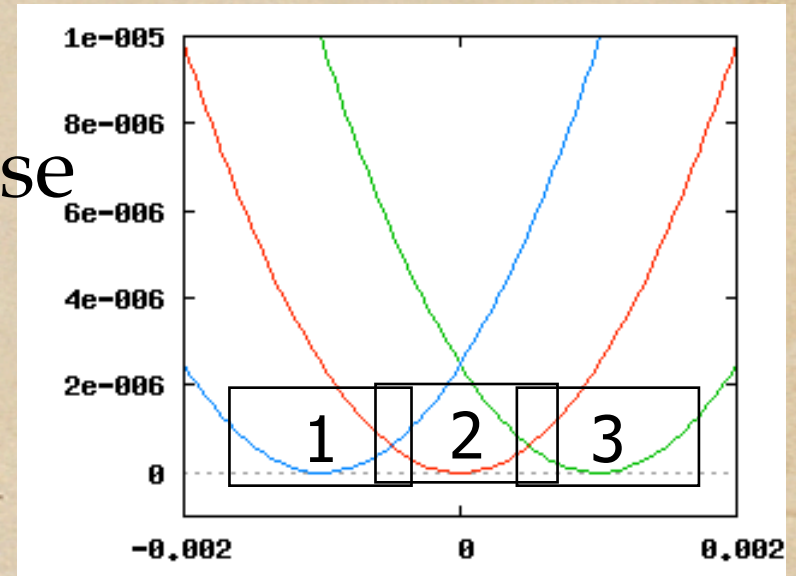
$$< 3.0 \times 10^{-7}$$

No DC System.

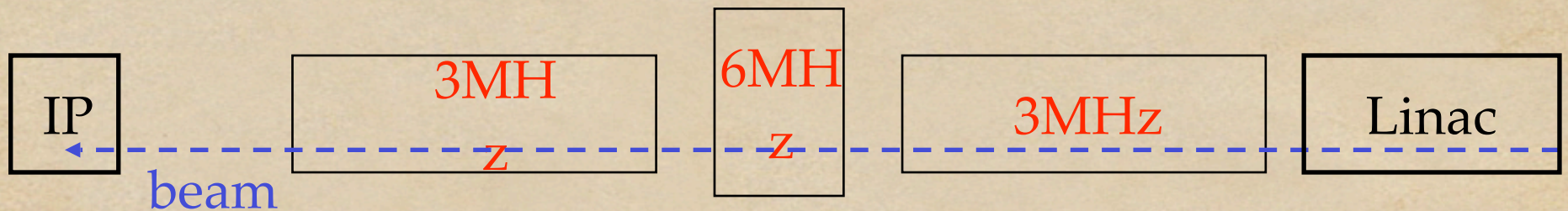
Not at the center

Compensation by Phasing

- ◆ Phasing = different phase at each section.
- ◆ Apply each bottom to incoming beam
- ◆ No need for 133 division
→ divide into **some group**



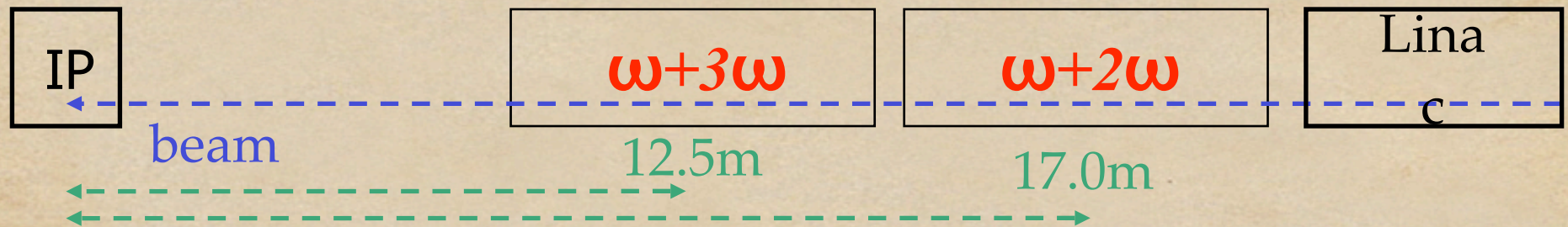
Advantage of sine option



- ◆ Can apply the harmonics separately.
- ◆ Waveform $\omega+2\omega$ needs 2 groups
 - Separate RF's are useful for

Easier construction & Phasing

Expansion: 500GeV \rightarrow 1TeV



- ◆ Kicker's location depends on the harmonics.
→ multiple kickers can distribute.
- ◆ Operate 1 kicker for 500GeV
- ◆ Operate 2 kickers for 1TeV

RF Stability

- ◆ Amplitude jitter $\sim 10^{-2}$ has little effect
- ◆ Phase fluctuation is dominant.

for 2 grouped separate RF system,

phase	1×10^{-3}	4×10^{-3}	1×10^{-2}	3×10^{-2}	[rad]
$\omega+2\omega$	1.00	1.15	1.50	3.16	$\times 10^{-7}$ [rad]
$\omega+3\omega$	2.59	2.99	3.89	8.20	$\times 10^{-7}$ [rad]

Phase stability within 10^{-3} rad is desirable.

Issues on RF kicker

- ◆ More investigation on material for kicker core (FINEMET)
- ◆ Investigate for vertical kick by fringing field
- ◆ Beam chamber has to be made of insulator.
<Shield by thin metal(copper)?>
- ◆ Estimated RF power: 45kWpk/core,
(0.25Tx4m, 1mrad) x (133 cores, 133 Amp's)
- ◆ Dark current issue
- ◆ Abort kicker (MPS)
- ◆ Septum Magnet ?
- ◆ BPM? (directional BPM?)